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Patent- und Rechtsanwälte

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(54) **Method of liquefying paper, liquefied paper composition and method of manufacturing plastic molding from liquefied paper composition**

(57) Disclosed is a method of liquefying a paper material, a liquefied paper composition and a method of manufacturing a plastic molding from a paper material by using the liquefied paper composition. The paper is shear broken into small pieces and mixed with a liquefying agent containing: an alkaline catalyst or an acidic catalyst; and at least one liquid compound which is selected from the group consisting of hydroxyphenyl compound, polyol and cyclic ester. The mixture is heated to obtaining a liquefied paper composition. Iso-cyanate compound or a curing agent for phenol resins is added to the liquefied paper composition and the mixture is molded to form the plastic molding, which is usable in place of conventional plastic articles.

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Description

BACKGROUND OF THE INVENTION

5 Field of the Invention

[0001] The present invention relates to a method of liquefying a used paper material, a liquefied paper composition obtained by the liquefying method, and a method of manufacturing a plastic molding using the liquefied paper composition; for efficiently manufacturing a plastic molding which is replaceable with a conventional plastic molding.

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Description of the Prior Art

[0002] The resources on the earth have been used by the humankind to create various products, in order to improve and enrich their lives. For example, the wood resources have been utilized to manufacture paper materials which are applied to news papers, magazines, recording media which are to be used in OA (office automation) devices and the like, and the fossil resources such as petroleum and the like have been utilized to manufacture plastic moldings and other chemical products. In this connection, there is a steady increase in the amount of the fossil resources consumed for manufacturing the products, and it has reached at present an enormous amount. However, the natural resources are in fact limited, though people tend to have such hallucination that they were rich enough and endless. In view of environmental protection and use of resources with advantage, it is therefore earnestly desired to reduce consumption of the resources and promote recycle of the used resources. In the circumstances as described above, it is being proceeded to develop the recycling technology for various resources.

[0003] However, recycling of plastic moldings as a fossil resource includes various problems and they seem not to be easily solved for technical and economical reasons. Therefore, recovering and reclamation of plastic moldings are not satisfactorily carried out. Moreover, the plastic moldings that can be reclaimed comprise only a limited part of the whole plastics. Accordingly, even if recovering of the plastics are advanced to raise the recycling ratio in comparison with the present time, the amount of fossil resource required for manufacturing moldings will not fall very much and it will be therefore difficult to decrease the consumption of the fossil resource.

[0004] On the other hand, as to the wood resources, the technique for reclaiming used paper has been established and it has been recommended to recover the used paper such as paper sheets recorded by office automation devices, news paper, magazines and the like, in order to spread the recycle of reclaimed paper. However, due to the problem of the cost for treatments which are carried out at the paper reclamation, such as removal of printed ink and the like, the amount of used paper which is effectively utilized for reclamation is possibly reduced to no more than a part of the whole of the recovered paper. Accordingly, a large amount of extra used paper may remain after the recycle. If such a state continues for a long time, recycle of used paper cannot help being inhibited, resulting in placing a large obstacle in the way of efficient utilization of the wood resources.

[0005] In the circumstances as described above, there are demands for activation of recycle by developing technique which enables application of a resource to a novel recycling use to accelerate circulation of resources, in particular, recycling technique which enables to recycle one resource as another resource, in order to increase the efficiency in utilization of natural resources.

SUMMARY OF THE INVENTION

[0006] With these problems in mind, therefore, it is the primary object of the present invention to provide a novel recycling technique which enables crossover recycling between different resources, and in which an extra part of the recovered used paper is used in a novel recycling use to activate the recycling, thereby the paper resource can be sufficiently recycled.

[0007] Moreover, it is the secondary object of the present invention to provide a crossover recycling technique which enables to convert a non-plastic material to a material for manufacture of plastic products.

[0008] In order to achieve the above-mentioned object, a method of liquefying a paper material, according to the present invention, comprises the steps of: shear breaking the paper material into small pieces of paper; mixing the small pieces of paper with a liquefying agent comprising: an alkaline catalyst or an acidic catalyst; and at least one liquid compound which is selected from the group consisting of hydroxyphenyl compound, polyol and cyclic ester, to obtain a mixture; and heating the mixture, thereby obtaining a liquefied paper composition.

[0009] In the liquefying method, the used paper material is broken at the shear breaking step so that the length of the longest side of each piece of the broken paper is at least 50 % by weight of the broken paper is 5 mm or less.

[0010] In one aspect of the invention, the paper material is broken at the shear breaking step so that the paper fibers of the broken paper are not raised, and the length of the shortest side of each piece of the broken paper is at least 50

% by weight of the broken paper is 0.5 mm or less.

[0011] In another aspect, the paper material is pulp sludge, and the paper material is cut at the shear breaking step so that the ratio of paper fibers having a length of 1 mm or more is reduced to 20 % by weight or less.

[0012] In further aspect, the paper material includes at least one material from the group consisting of coated paper, resin-composited paper and shredded paper, and the mixing step and the heating step are performed by using an extruder.

[0013] Moreover, a liquefied paper composition, according to the present invention, comprises: a liquid compound which is selected from the group consisting of hydroxyphenyl compound, polyol and cyclic ester; and a liquefied matter of paper fibers, wherein the ratio of a paper residue in the liquefied paper composition is 20 % by weight or less.

[0014] Moreover, a method of manufacturing a plastic molding from a paper material by using the liquefied paper composition obtained by the above-described liquefying method comprises the steps of: mixing the liquefied paper composition with isocyanate compound and a urethane polymerization catalyst or with a curing agent for phenol resins; and molding the mixture of the liquefied paper composition into the plastic molding.

BRIEF DESCRIPTION OF THE DRAWINGS

[0015] The features and advantages of the paper liquefaction method, the liquefied paper composition and the manufacturing method of plastic moldings from a paper material according to the present invention over the conventional method will be more clearly understood from the following description of the preferred embodiments of the present invention taken in conjunction with the accompanying drawing.

Fig. 1 is a schematic view showing the broken paper pieces according to the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0016] The inventors of the present application have performed various researches about solution of the above-described problems. As a result, they have found that it is possible to efficiently liquefy the used paper, and to manufacture a plastic moldings having good quality with use of the liquefied paper.

[0017] Now, preferred embodiments of the method of liquefying paper, of the liquefied paper composition obtained by the liquefaction method, and of the manufacturing process of a plastic molding from the liquefied paper composition according to the present invention will be described.

[0018] Generally, paper is manufactured, using pulp which comprises cellulose fibers of wood or other plants and the main body of paper is composed of lignocellulose ("lignocellulose" is used as a generic designation including cellulose, hemicellulose and lignin). As for the wooden material, there is a conventional liquefaction method of liquefying lignocellulose and preparing a resin therefrom, and it is known from the publication documents of Japanese Laid-Open Patent No. S61-261358, Japanese Laid-Open Patent No. S62-79230 and Japanese Laid-Open Patent No. H8-225653.

[0019] However, the conventional liquefying method described above is unsuitable for practicing liquefaction of paper lignocellulose and manufacture of a plastic molding from the liquefied material. Namely, a few serious problems arise to hinder the practice of it.

[0020] Specifically, the first problem resides in that it takes a quite long time with the conventional liquefaction method to liquefy merely a small amount of wood lignocellulose on an experimental scale. Accordingly, it is impossible to cope with industrial production on a large scale. Moreover, the object of the conventional liquefaction method is a wooden material which is different from paper in composition and organic structure, and it is therefore unadaptable to liquefaction of a paper material.

[0021] The second problem resides in that, since paper is an aggregate of fibers and has a structure with high ability to hold the air therein, it is easily hindered by the remaining air from contacting with a liquefying agent which has great viscosities. In this connection, there is another hinderance by various additives such as dyestuff, coating materials and the like, which are applied to the paper in order to impart an appropriate function required in accordance with its utility. These additives also hinder the paper from contacting with the liquefying agent to often inhibit the advance of liquefaction. Furthermore, the fibers in paper are tightly piled up to make a pretty large density, and that is another reason of a low liquefaction rate per unit weight of paper and a long time that is necessary for liquefaction.

[0022] In short, a matter of importance in practice of liquefaction of paper as a recycling technology resides in that liquefaction must be realized with high efficiency on an industrial production scale for treatment of a large amount of paper. In order to achieve this purpose, it is proposed according to the present invention that paper is broken into small pieces like fish scales or other like things, and the broken paper are put into a liquefying agent containing a catalyst for liquefying those pieces of paper, so that the pieces of paper easily contact with the liquefying agent and the liquefaction rate per unit weight is improved. A purpose of breaking the paper to be treated into pieces is to increase the ratio, per unit weight paper, of the surface area on which the paper may contact with the liquefying agent, and to reduce the hin-

derance from contacting with the liquefying agent which is caused by a coating material on the surface of paper or the like. Moreover, it is another purpose to develop penetration of the liquefying agent from the cut section along the paper fibers into the paper.

[0023] Since common paper has a pretty large density, paper can be formed into particles having extremely high movability or fluidability by breaking it into small pieces. It also becomes easy to mix the paper with the liquefying agent which is highly viscous, due to reduction of contact hinderance. Moreover, workability at the step of placing the paper into the liquefying agent is remarkably improved by good fluidability of the paper particles. Particularly, when liquefaction is operated by using an extruder which is capable of enhancement of liquefaction reaction by pressing and mixing and of continuous processing, breaking of the paper into pieces is a great influence upon whether the liquefaction is possibly realized or not. In other words, it is quite important to break into small pieces the paper to be liquefied, for liquefaction with an extruder which is quite promising for practical recycle of paper as a material for plastic reproduction. This matter is also an advantageous feature for enabling to advance effective recycle of the used paper which is shredded under the necessity of information management and which cannot help being abandoned because of reclamation of shredded paper being impossible.

[0024] It is unnecessary to restrict the kind of paper which is used as a starting material for manufacturing liquefied lignocellulose. As examples of the starting material illustrated are paper sheets used in office automation devices, news paper, magazine paper, cardboard, wrapping paper, thermosensible paper, coated paper, resin-composite paper and the like, and pulp materials such as pulp sludge and the like can also be included in the starting material. As described above, it is possible to suitably use shredded paper as a material. Coated paper is a paper material that a coating is applied on the surface of a paper base and it is often used for a cover page of magazines, a poster, a catalogue, a pamphlet and the like. The resin-composite paper is a paper material which a layer of resin is adhered or laminated on the surface of a paper base or incorporated in the paper base. In either case of the coated paper and the resin-composite paper, it is required for paper recycle by the conventional method to remove the coating or the resin.

[0025] The raw paper is broken with shearing action into pieces as small as possible. Preferably, it is shear-cut in such a manner that, as shown in FIG. 1, the length L of the longest side of each paper piece in at least 50 % of the broken paper pieces 1, 2 is about 5 mm or less, preferably about 2 mm or less. As a better mode, it is further desired that the length S of the shortest side (or thickness) is 0.5 mm or less, preferably about 0.2 mm or less. If the raw paper is thick, it is cut smaller, accordingly. It is preferred that the paper pieces have a simple shape that has substantially no complication by projection and concavity, and preferable shapes are, for example, a rectangular solid or strip, a fish scale-like slice, a circular disk, a rod and the like. If the paper pieces have a complicated shape with projections and concavities, they are easily entangled in each other and the fluidity of paper pieces comes down. As a result, the air is held in the concavities or gaps between the paper pieces and easily inhibits the paper pieces from contacting with the liquefying agent. The device used for cutting the paper is desirably a breaking device using shearing action, such as a shredder, a milling cutter and the like. In these breaking devices, breaking is performed in the style of cutting or shearing with cutting blades. In a condition like those, the fibers of paper are appropriately cut so that the broken pieces of paper are prevented from gitting at the cut section like cotton rags.

[0026] The broken paper obtained by the above breaking operation is rather dense, and it has, in general, a bulk density of about 0.1 g/cm³ or more.

[0027] If the paper is cut into larger dimensions than the preferable dimensions described above, the bulkiness of the paper pieces and the volume of the air held between the paper pieces increase, which produces hindrance when putting a large amount of paper pieces into an extruder and controlling the amount of paper pieces put into it. Moreover, uniformity in quality of the liquefied product is reduced and quality of the plastic product manufactured from the liquefied product is not kept constant. If cutting ability of the used cutting instruction is poor, the fibers of paper are loosened at the cut section of the paper pieces and gitting is caused to make the paper pieces bulky like cotton rags. As a result, the paper pieces may be, in some case, entangled with each other by the raised fibers to make a lump of paper pieces. In such a state, it is difficult not only to put the paper pieces into the extruder, but also to penetrate the liquefying agent into the spaces between the lumped paper pieces. Accordingly, liquefaction reaction does not uniformly proceed, and this makes inconstant quality of the liquefied product. In a case where the paper is in a state in which the paper fibers are loosened like raw cotton or raised and entangled to make lumps, or in a case of pulp sludge, the paper should be cut using a shearing machine such as a shredder, milling cutter, etc. so that the ratio of fibers having a length of 1 mm or more is reduced to 20 % or less, desirably 10 % or less, before starting the liquefaction treatment. According as the amount of fibers having a length of 1 mm or more increase, the paper pieces easily make lumps.

[0028] As understood from the above description, the used paper ordinarily recovered from the users can be liquefied after breaking into pieces having a shape as described above.

[0029] The paper to be liquefied may contain a wood powder or a starch such as corn, rice and the like. Moreover, it may be mixed with a filler made of a powder of silica, alumina, talk or the like and having a particle size of 5 μ m or less, in order to improve the fluidability of the raw material at the liquefaction step.

[0030] The paper pieces broken as described above are added to the liquefying agent and then heated, thereby

obtaining a liquefied matter of lignocellulose. The liquefying agent is a liquidus mixture comprising: an alkaline or acidic catalyst; and at least one liquidus compound which is selected from the group consisting of hydroxyphenyl compounds, polyols and cyclic esters. The alkaline or acidic catalyst is used at an amount sufficient for developing the liquefaction reaction. An suitable example of the liquefying agent comprises the alkaline or acidic catalyst at a ratio of 0.2 to 10 %
 5 by weight relative to the paper pieces, and the liquidus compound at a ratio of 50 to 300 % by weight relative to the paper pieces. Preferably, the ratio of the catalyst to the paper pieces is 1 to 5 % by weight, and the ratio of the liquidus compound to the paper pieces is 80 to 200 % by weight.

[0031] For the hydroxyphenyl compound, phenol, cresol, xylenol, resorcinol, acrylic resorcinol, bisphenol A and the like can be suitably used, but it should not be limited to these compounds.

[0032] For the polyols, illustrated are, for example, bivalent alcohol such as ethylene glycol, propylene glycol, trimethylene glycol, 1,4-butanediol, 1,5-pentanediol, 1,6-hexanediol, 1,2-hexanediol, 2,4-hexanediol, 1,7-heptanediol, 1,8-octanediol, 1,9-nonanediol, 1,10-decanediol, pinacol, cyclopentane-1,2-diol, cyclohexane-1,4-diol, polyethyleneglycol, polyoxypropyleneglycol, polyoxypropylene-polyoxyethylene glycol and the like; and trivalent or polyvalent alcohol such as glycerin, trimethylolpropane, triethanolamine, 1,2,6-hexanetriol, pentaerythritol, methyl glucoside, sorbitol,
 15 mannitol, sucrose and polyether polyol partially containing a polycaprolacton in which either of the above described polyol compounds is a starting material, and the like. However, the polyol in the present invention should not be limited to the above-described compounds. Among these compounds, a mixture of glycerin and polyethyleneglycol is cheap and industrially available. Therefore, this mixture is especially suitable to use for the liquefaction of paper according to the present invention.

[0033] For the cyclic esters, such compounds that are able to make ring opening reaction and polymerize is suitable. For example illustrated are propiolactone, β -butyrolactone, α,α' -bischloromethylpropiolactone, α,α -dimethyl- β -propiolactone, δ -valerolactone, 1,4-dioxane-2-on, glycolide, trimethyl carbonate, neopentyl carbonate, ethylene oxalate, propion oxalate, ϵ -caprolactone, α -methyl- ϵ -caprolactone, β -methyl- ϵ -caprolactone, γ -methyl- ϵ -caprolactone, 4-methyl-7-isopropyl- ϵ -caprolactone, 3,3,5-trimethyl- ϵ -caprolactone, cis-disalicylide, trisalicylide and the like. However, it should
 25 not be limited to the above-described compounds. Among these compounds, ϵ -caprolactone is cheap and industrially available. Therefore, this compound is especially suitable to use for the liquefaction of paper according to the present invention.

[0034] For the alkaline catalyst illustrated are, for example, alkaline metal hydroxide such as sodium hydroxide, potassium hydroxide and the like; alkaline-earth metal hydroxide such as calcium hydroxide and the like; alkaline-earth metal carbonate such as calcium carbonate and the like; and ammonia and amino compounds such as monoethanolamine and the like. However, it should not be limited to these compounds.

[0035] The acidic catalyst includes, for examples, inorganic acid compounds, organic acid compounds, Lewis acid compounds and the like. Specifically, sulfuric acid, hydrochloric acid, toluensulfonic acid, phenol sulfonic acid, aluminum chloride, zinc chloride, boron trifluoride and the like can be preferably utilized for the acidic catalyst. However, it
 35 should not be limited to the above examples.

[0036] For advancing the liquefaction of paper, mixing operation such as stirring or kneading is necessary and it is preferred to use an apparatus possessing a heating function and a mixing function. In a case where bulk production capacity and efficiency are further required, use of an extruder is desirable because continuous liquefaction is possible with it and pressuring and stirring are possibly performed during the liquefaction treatment. In this case, a mixture of the
 40 paper and the liquefying agent is suitably put into the extruder and kneaded while it is heated. Use of a twin-screw extruder in which the raw paper may be further broken into smaller pieces is preferable because the liquefaction efficiency is remarkably raised.

[0037] The heating temperature during the liquefaction treatment is within a range of 100 to 200 °C, preferably 150 to 190 °C. The time necessary for the liquefaction varies depending on the degree of stirring or kneading. However, an appropriate liquefaction time, as an example, can be illustrated as being 5 to 20 minutes for a case where stirring at the
 45 rate of 5 to 150 rpm is performed in the extruder.

[0038] In accordance with the liquefaction operation as described above, a paper material is liquefied.

[0039] The liquefied paper obtained above, i.e., the liquefied paper composition containing liquefied lignocellulose, is mixed with a neutralizer to use as a raw material of chemical products. Specifically, it is used for manufacturing a urethane coating, a urethane adhesive or the like. Alternatively, it may be mixed with an isocyanate compound and a polymerization catalyst, and, as necessity arises, further mixed with a surfactant, a foaming agent, a foam stabilizer, a filler and the like, to mold the mixture, thereby it is possible to manufacture various products such as cushioning materials, thermal insulation materials, construction materials, automobile parts of molding by RIM (Reaction Injection Molding) or R-RIM (Reinforced Reaction Injection Molding), various elastomers and flooring materials, etc. In this
 55 connection, the usable isocyanate compound may generally include isocyanate compounds having at least two isocyanate (-NCO) groups, and, in particular, use of MDI (diphenylmethane-4,4'-diisocyanate), TDI (tolylene diisocyanate), NDI (1,5-naphthalene diisocyanate) or H12MDI (hydrogenated MDI) is preferred.

[0040] In a case where paper is liquefied with use of a hydroxyphenyl compound, the liquefied paper may be hard-

ened by adding a curing agent ordinarily used for phenolic resins.

[0041] Liquefaction of lignocellulose starts from the paper surface being contacting with the liquefying agent. If the liquefaction efficiency is low, a large amount of paper residue remains in the liquefied product. However, in the present invention, the ratio of the paper residue to the raw paper (this is measured for water-insoluble matters as described in EXAMPLES) is reduced to 30 % by weight or less after 5 to 20 minutes of liquefaction treatment, in accordance with the construction that paper is broken with shear action into small pieces before liquefaction and the paper pieces are kneaded by an extruder during the liquefaction. As a result, it is made possible to obtain a liquefied lignocellulose product in which the content of paper residue is about 20 % by weight or less. Moreover, the dimensions of the paper residue remaining in the liquefied product becomes smaller by breaking the paper to be liquefied into small pieces. Therefore, quality of the plastic product manufactured from the liquefied product is improved as well.

[0042] As described above, it is possible to efficiently manufacture a large volume of liquefied product from paper materials by a continuous treatment at a low cost, in accordance with the above-described liquefaction method. At the same time, the liquefied product obtained therefrom has uniform quality so that it is possible to manufacture plastic product without dispersion.

EXAMPLES

[0043] Examples of the liquefaction of paper according to the present invention will now be described in detail below. Here, it is to be noted that each of the units, "%" and "part", is used as that expressed by weight, respectively, in this section.

(Example 1)

[0044] Used paper sheets (A4 size) recovered from OA devices were put into a shear-cutting type cutting machine (code: JC-5 type, manufactured by Morita Seiki Industrial Co., Ltd. of Saitama, Japan) equipped with a screen with openings having a diameter of 2 mm, to obtain pieces of used paper. In 99 % or more of the pieces of used paper, the length of the longest side of the piece was 2 mm or less and the thickness was 0.2 mm or less.

[0045] A bench extruder (manufactured by Harada Seisakujo of Tokyo, Japan) having a charge hopper in which the bore diameter was 20 mm was heated to adjust the temperature to 170 °C, and 100 parts of the used paper pieces obtained above were put into the bench extruder together with 140 parts of polyethylene glycol (average molecular weight: about 400), 60 parts of glycerin and 6 parts of sulfuric acid (concentration: 97 %) through the charge hopper. The velocity of rotation of the screw of the bench extruder was low-rate of 13 rpm.

[0046] After 15 minutes passed from the charging, a black-colored liquefied product began to flow out continuously from a nozzle of the bench extruder. The liquefied product obtained above was subjected to measurement of the percent residue, the percent residue content and the viscosity of the liquefied product in accordance with the following methods. The results of the measurement are shown in Table 1.

[measurement of the residues of the paper and of the liquefied product]

[0047] First, 2 g of the liquefied product was diluted with ion-exchange water and sufficiently stirred to dissolve liquefied paper into water, thereby preparing a dilute solution of the liquefied paper. Next, using a filter paper which had been completely dried and weighed in advance, the dilute solution of the liquefied paper was filtered. The filter paper after the filtration was dried at 110 °C to a constant weight. From the weight values of the filter paper before and after the filtration, the weight of the residue, which included unliquefied paper and insoluble matters by incomplete liquefaction, was obtained, and the percent residue and the percent residue content were calculated by the following equations.

$$\text{percent residue (\%)} = \frac{\text{weight (g) of residue}}{\text{weight (g) of raw paper}} \times 100$$

$$\text{percent residue content (\%)} = \frac{\text{weight (g) of residue}}{\text{weight (g) of liquefied product}} \times 100$$

[measurement of the viscosity of liquefied product]

[0048] The liquefied product in a glass tube of 40 Ømm was placed in a thermostatic bath in which the temperature was controlled to 80 °C, and the viscosity of the liquefied product being kept to a constant temperature was measured by a B type viscometer (manufactured by Toki Industry Co., Ltd. of Tokyo, Japan).

(Examples 2 and 3)

[0049] In each of Examples 2 and 3, the procedure of Example 1 was repeated, excepting that the amount of the used paper pieces put into the bench extruder was changed to 150 parts (Example 2) or 200 parts (Example 3), to obtain a liquefied product. The liquefied product was similarly subjected to measurement of the percent residue, the percent residue content and the viscosity of the liquefied product. The results of the measurement are shown in Table 1.

(Examples 4 and 5)

[0050] In each of Examples 4 and 5, the used paper was broken into pieces by the same manner as Example 1.

[0051] A twin-screw extruder (code: TEM-37BS, manufactured by Toshiba Machine Co., Ltd. of Tokyo, Japan) was set for liquefaction of the used paper pieces so that the cylinder temperature of the extruder was raised to 180 °C and the rotational velocity of the screws was adjusted to 30 rpm. Into the twin-screw extruder, 150 parts (Example 4) or 200 parts (Example 5) of the used paper pieces, 140 parts of polyethylene glycol (average molecular weight: about 400), 60 parts of glycerin and 6 parts of sulfuric acid (concentration: 97 %) were put into the extruder through the a charging hopper in such a manner that the feed rate of the used paper pieces to the extruder was 3.6 kg/hour.

[0052] After 15 minutes passed from the charging, a black-colored liquefied product began to flow out continuously from the nozzle of the extruder. The liquefied product obtained above was subjected to measurement of the percent residue, the percent residue content and the viscosity of the liquefied product in the same manners as Example 1. The results of the measurement are shown in Table 1.

(Example 6)

[0053] Used Paper sheets (A4 size) recovered from OA devices were put into a shredder to obtain paper strips having a width of 5 mm. The paper strips were further broken by a desk-type crusher. Since the broken paper formed a mass of paper pieces in which paper fibers were raised and entangled like cotton wool, it was further cut by a shear-cutting type cutting machine (code: JC-5 type, manufactured by Morita Seiki Industrial Co., Ltd. of Saitama, Japan) equipped with a screen with openings having a diameter of 1 mm. The cut pieces of used paper obtained above were fluid in a state of powder in which there was not seen entangled fibers. Observing the pieces of used paper under a microscope, 16.3 % of the pieces of used paper had the longest side being 1 mm or more.

[0054] A bench extruder (manufactured by Harada Seisakujo of Tokyo, Japan) having a charging hopper in which the bore diameter was 20 mm was heated to adjust the temperature to 170 °C, and 100 parts of the used paper pieces obtained above were put into the bench extruder together with 140 parts of polyethylene glycol (average molecular weight: about 400), 60 parts of glycerin and 6 parts of sulfuric acid (concentration: 97 %) through the charging hopper. The rotation velocity of the screw of the bench extruder was low rate of 13 rpm.

[0055] After 15 minutes passed from the charging, a black-colored liquefied product began to flow out continuously from the nozzle of the bench extruder. The liquefied product obtained above was subjected to measurement of the percent residue, the percent residue content and the viscosity of the liquefied product in the same manners as Example 1. The results of the measurement are shown in Table 1.

[0056] As shown in Table 1, the percent residue and the viscosity of the liquefied product were 7.5 % and 38 P, respectively, and the quality of the liquefied product was suitable for use.

Table 1

Example	1	2	3	4	5	6
paper (part)	100	150	200	150	200	100
polyethylene glycol (part)	140	140	140	140	140	140
glycerin (part)	60	60	60	60	60	60
sulfuric acid (part) [conc. 97%]	6	6	6	6	6	6
percent residue (%)	8	11	16	10	14	7.5
percent residue content (%)	2.6	4.2	8	4.2	7	2.5
viscosity (P)	41	60	186	45	122	38

(Comparative Example 1)

[0057] Used Paper sheets (A4 size) recovered from OA devices were put into a shredder to obtain paper strips having a width of 5 mm. The paper strips were further cut with scissors. Of the cut pieces of used paper obtained above, the ratio of pieces that the length of the longest side was 5 mm or less was less than 1 %.

[0058] A bench extruder (manufactured by Harada Seisakujo of Tokyo, Japan) having a charging hopper in which the bore diameter was 20 mm was heated to adjust the temperature to 170 °C, and the rotational velocity of the screw of the bench extruder was low-rate of 13 rpm. Moreover, 100 parts of the used paper pieces obtained above were mixed with 140 parts of polyethylene glycol (average molecular weight: about 400), 60 parts of glycerin and 6 parts of sulfuric acid (concentration: 97 %), and the mixture was put into the charging hopper of the bench extruder. However, it was difficult to feed the mixture into the extruder and most part of the mixture was remaining at the charging hopper, so that liquefaction of paper did not proceed. The rotational velocity of the screw was changed gradually from 13 rpm up to 30 rpm. However, there was few change in feeding of the mixture into the extruder.

(Comparative Example 2)

[0059] The procedure of Comparative Example 1 was repeated, excepting that, instead of the bench extruder, a twin-screw extruder (code: TEM-37BS, manufactured by Toshiba Machine Co., Ltd. of Tokyo, Japan) in which the cylinder temperature of the extruder was raised to 180 °C and the rotational velocity of the screws was adjusted to 60 rpm was used. However, it was difficult to feed the paper mixture into the extruder and most part of the mixture was remaining at the charging chopper, so that liquefaction of paper did not proceed. The rotational velocity of the screw was changed gradually from 60 rpm up to 100 rpm. However, there was few change in feeding of the paper mixture into the extruder.

(Comparative Example 3)

[0060] Used Paper sheets (A4 size) recovered from OA devices were put into a shredder to obtain paper strips having a width of 5 mm. The paper strips were further broken by a desk-type crusher. The broken paper formed a lump of paper pieces in which paper fibers were raised at the broken edges and entangled like cotton wool.

[0061] A bench extruder (manufactured by Harada Seisakujo of Tokyo, Japan) having a charging hopper in which the bore diameter was 20 mm was heated to adjust the temperature to 170 °C. Moreover, 100 parts of the used paper pieces obtained above were mixed with 140 parts of polyethylene glycol (average molecular weight: about 400), 60 parts of glycerin and 6 parts of sulfuric acid (concentration: 97 %), and this paper mixture was put into the charging hopper of the bench extruder. The screw of the bench extruder was then rotated at a low rate of 13 rpm. During the charging, since the charging hopper was often choked with the paper mixture, the extruder was stopped at every occurrence of choking in order to manually push the paper mixture into the extruder. The liquefied product flew out of the extruder had unliquefied paper spots having a dimension of about 1 mm. Therefore, liquefaction did not sufficiently proceed.

(Comparative Example 4)

[0062] Used Paper sheets (A4 size) recovered from OA devices were put into a shredder to obtain paper strips having a width of 5 mm. The paper strips were further cut with scissors. Of the cut pieces of used paper obtained above, the ratio of pieces that the length of the longest side was 5 mm or less was less than 1 %.

[0063] Then, 100 parts of the used paper pieces obtained above were mixed with 140 parts of polyethylene glycol (average molecular weight: about 400), 60 parts of glycerin and 6 parts of sulfuric acid (concentration: 97 %), and the mixture was put into a kneader (code: KM-5 type, manufactured by Dalton of Japan) and heated at 150 °C for 1 hour while the mixture was stirred. During the stirring, the paper strips were entangled in each other and were sometimes engaged between the kneader blade and the container to stop the operation with alarming.

[0064] After the above operation, the liquefied product was obtained in a liquid state but unliquefied paper pieces which could be visually recognized were remaining.

[0065] The liquefied product was subjected to measurement of the percent residue and the percent residue content of the liquefied product in the same manners as Example 1. As a result, the percent residue was 60 % and the percent residue content was 19.6 %.

(Example 7)

[0066] To 100 parts of the liquefied product obtained in Example 4, 4 parts of imidazol and 2 parts of a foam stabilizer (code: SZ-1627, manufactured by Nippon Unicar Co., Ltd. of Tokyo, Japan) were added and the mixture was vig-

orously stirred for 20 seconds. Moreover, this mixture was further mixed with 75 parts of isocyanate (code: MDI-100, manufactured by Nippon Polyurethane Industry Co., Ltd. of Tokyo, Japan) and vigorously stirred for 10 seconds. The mixture was poured into a mold which had been previously prepared, thereby obtaining moldings. The moldings had a sufficient quality for the cushioning material.

- 5 **[0067]** In accordance with the above method, it was also possible to form a flame of interior light fitment, a damper and a cushioning material for interior automotive trims similarly from the liquefied product.

(Example 8)

- 10 **[0068]** A mass of used paper which included news papers, magazines and shredded paper strips recovered from OA devices was placed in a tank made of iron. Water was poured into the tank and it was slowly stirred overnight. The liquid containing loosened paper fibers was pumped up from the tank and dried to obtain a mass of dried paper fibers. It was placed in an oven to further dry it up. The mass of paper obtained above was put into a shear-cutting type cutting machine (code: JC-5 type, manufactured by Morita Seiki Industrial Co., Ltd. of Saitama, Japan) equipped with a screen
15 with openings having a diameter of 1 mm, to break the paper. The broken paper was in a state of fluidic powder in which paper fibers were not entangled. Observing the broken paper under a microscope, 7.4 % of the broken paper were paper fibers having a length exceeding 1 mm.

- [0069]** Then 100 parts of the broken paper obtained above was mixed with 100 parts of phenol and 3 parts of sulfuric acid and the mixture was poured into a bench extruder (manufactured by Harada Seisakujo of Tokyo, Japan) which
20 was heated to 150 °C and operated for 1 hour, to obtain a liquefied product. The liquefied product was subjected to the measurement of the percent residue described in Example 1. As a result, the percent residue was 8.2 %. When the liquefied product was left to stand at a room temperature, it was solidified.

- [0070]** Into a Henschel mixer, 100 parts of the solidified product obtained above, 100 parts of silica powder (trade name: NA1, manufactured by Tatsumori Co., Ltd. of Tokyo, Japan) having an average particle size of 10 µm, 50 parts
25 of glass fiber chopped strand (Nippon Sheet Glass Co., Ltd. of Tokyo, Japan) having a length of 1mm, 2 parts of carnauba wax, 6 parts of calcium hydroxide and 25 parts of hexamethylenetetramine as a curing agent were placed and mixed with each other. The mixture was heated to 120 °C and the molten mixture was kneaded for 1 minute with a pair of rolls. The molten mixture was then cooled to a room temperature to solidify it. It was further pulverized and compressed into tablets having dimensions of 10 Ø x 10 mm.

- 30 **[0071]** Using the tablets obtained above as a material for press molding, it was able to produce a substrate for printed wiring boards, a case of personal computers, a case of cellular phones and the like. Each of the press-molded products had a favourable appearance and satisfied requirements for practical use.

- [0072]** As clearly understood from the above description, it is possible, according to the present invention, to efficiently prepare a liquefied paper composition from a used paper material at a low cost through a continuous extrusion
35 line. Moreover, it is possible, by using the liquefied product, to practically form various plastic moldings of high usefulness. Accordingly, recycling applicability of used paper is enlarged and consumption of the fossil resource is reduced. Therefore, liquefaction of paper according to the present invention has a great value for reservation and use with advantage of natural resources.

- 40 **[0073]** It must be understood that the invention is in no way limited to the above embodiments and that many changes may be brought about therein without departing from the scope of the invention as defined by the appended claims.

Claims

- 45 1. A method of liquefying a paper material, comprising the steps of:
- shear breaking the paper material into small pieces of paper;
 - mixing the broken paper with a liquefying agent comprising: an alkaline catalyst or an acidic catalyst; and at least one liquid compound which is selected from the group consisting of hydroxyphenyl compound, polyol and
50 cyclic ester, to obtain a mixture; and
 - heating the mixture, thereby obtaining a liquefied paper composition.
2. The liquefying method of claim 1, wherein the paper material is broken at the shear breaking step so that the length of the longest side of each piece in at least 50 % by weight of the broken paper is 5 mm or less.
- 55 3. The liquefying method of claim 1 or 2, wherein the paper material is broken at the shear breaking step so that the paper fibers of the broken paper are not raised, and the length of the shortest side of each piece in at least 50 % by weight of the broken paper is 0.5 mm or less.

4. The liquefying method of either of claims 1 to 3, wherein the mixing step and the heating step are performed by using an extruder.

5. The liquefying method of either of claims 1 to 4, wherein the paper material includes at least one material selected from the group consisting of coated paper, resin-composited paper and shredded paper.

6. The liquefying method of either of claims 1 to 5, wherein the paper material is pulp sludge, and the paper material is cut at the shear breaking step so that the ratio of paper fibers having a length of 1 mm or more is reduced to 20 % by weight or less.

7. The liquefying method of either of claims 1 to 6, wherein the liquefying agent of the mixing step comprises: the alkaline or acidic catalyst at a ratio of 0.2 to 10 % by weight relative to the broken paper; and the liquidus compound at a ratio of 50 to 300 % by weight relative to the broken paper, and the mixture at the heating step is heated at a temperature of 100 to 200 °C.

8. The liquefying method of either of claims 1 to 7, wherein the hydroxyphenyl compound is selected from the group consisting of phenol, cresol, xlenol, resorcinol, acrylic resorcinol and bisphenol A,

the polyol is selected from the group consisting of ethylene glycol, propylene glycol, trimethylene glycol, 1,4-butanediol, 1,5-pentanediol, 1,6-hexanediol, 1,2-hexanediol, 2,4-hexanediol, 1,7-heptanediol, 1,8-octanediol, 1,9-nonanediol, 1,10-decanediol, pinacol, cyclopentane-1,2-diol, cyclohexane-1,4-diol, polyethyleneglycol, polyoxypropyleneglycol, polyoxypropylene-polyoxyethylene glycol, glycerin, trimethylolpropane, triethanolamine, 1,2,6-hexanetriol, pentaerythritol, methyl glucoside, sorbitol, mannitol and sucrose,

the cyclic ester is selected from the group consisting of propionolactone, β -butyrolactone, α,α' -bischloromethylpropionolactone, α,α -dimethyl- β -propionolactone, δ -valerolactone, 1,4-dioxane-2-on, glycolide, trimethyl carbonate, neopentyl carbonate, ethylene oxalate, propion oxalate, ϵ -caprolactone, α -methyl- ϵ -caprolactone, β -methyl- ϵ -caprolactone, γ -methyl- ϵ -caprolactone, 4-methyl-7-isopropyl- ϵ -caprolactone, 3,3,5-trimethyl- ϵ -caprolactone, cis-disalicylide and trisalicylide,

the alkaline catalyst is selected from the group consisting of alkaline metal hydroxide, alkaline-earth metal hydroxide, alkaline earth metal carbonate, ammonia and amino compound, and

the acidic catalyst is selected from the group consisting of sulfuric acid, hydrochloric acid, toluensulfonic acid, phenol sulfonic acid, aluminum chloride, zinc chloride and boron trifluoride.

9. A liquefied paper composition, comprising:

a liquidus compound which is selected from the group consisting of hydroxyphenyl compound, polyol and cyclic ester; and

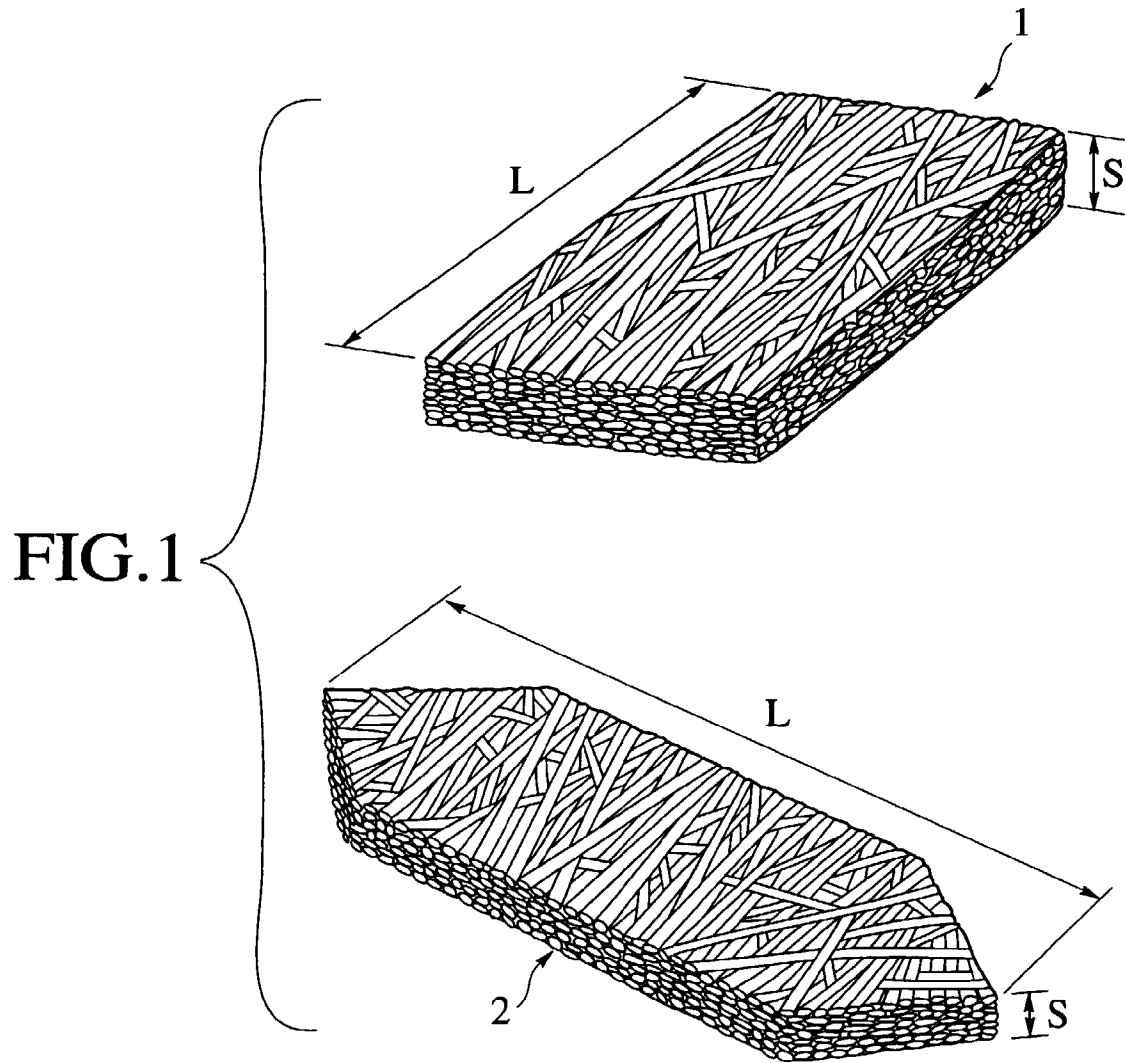
a liquefied matter of paper fibers,

wherein the ratio of a paper residue in the liquefied paper composition is 20 % by weight or less.

10. A method of manufacturing a plastic molding from a paper material by using the liquefied paper composition obtained by the liquefying method of either of claims 1 to 8, comprising the steps of:

mixing the liquefied paper composition with isocyanate compound and a urethan polymerization catalyst or with a curing agent for phenol resins; and

manufacturing a molding from the mixture of the liquefied paper composition.





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 00 10 5358

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
Y	US 5 110 915 A (TSUJIMOTO NAOHIKO ET AL) 5 May 1992 (1992-05-05) * column 3, line 20 - column 6, line 35; examples *	1,5,7-10	D21C5/02 B27N1/02 C08G18/64 C08L97/02 C08J5/04
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			D21C B27N C08G C08L C08J
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 22 June 2000	Examiner Bernardo Noriega, F
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document			

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**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 00 10 5358

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

22-06-2000

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DERWENT-ACC-NO: 2000-680971

DERWENT-WEEK: 200560

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TITLE: Method of liquefying broken paper
material for use in manufacture
of plastic moldings

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S ; THAI C M

PATENT-ASSIGNEE: TOSHIBA KK[TOKE]

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2000EP-105358 (March 17, 2000)

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EP 1036878 A1	September 20, 2000	EN
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DE 60002770 E	June 26, 2003	DE
JP 3696036 B2	September 14, 2005	JA

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JP 3696036B2	Previous Publ	2000JP- 076292	March 17, 2000

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CIPP	B09B3/00 20060101
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CIPS	B29B13/02 20060101
CIPS	C08G18/64 20060101
CIPS	C08L1/02 20060101
CIPS	C08L97/02 20060101
CIPS	D21B1/04 20060101
CIPS	D21C5/02 20060101
CIPS	D21J1/12 20060101

ABSTRACTED-PUB-NO: EP 1036878 A1

BASIC-ABSTRACT:

NOVELTY - Liquefying broken paper material comprises mixing with a liquefying agent and heating, the liquefied product being used in the manufacture of plastic moldings.

DESCRIPTION - A method of liquefying a paper material comprises (i) shear breaking the paper material into small pieces of paper; (ii) mixing the broken paper with a liquefying agent comprising an alkaline catalyst or an acidic catalyst, and at least one liquid compound selected from hydroxyphenyl compound, polyol and cyclic ester, to obtain a mixture; and (iii) heating the mixture to give a liquefied paper composition. Also claimed are (1) a liquefied paper composition comprising the above liquid compound and liquefied paper fibers, where the ratio of paper residue in the liquefied paper composition is 20 wt.% or less; and (2) manufacture of a plastic molding from a paper material comprising mixing the liquefied paper composition with an isocyanate compound and a urethane polymerization catalyst or a curing agent for phenol resins, and forming a molding.

USE - The plastic molding is usable in place of conventional plastic articles.

ADVANTAGE - The plastic molding is produced efficiently using crossover recycling techniques. Shredded paper can be recycled using the above

method. A large volume of uniform quality liquefied product can be manufactured by a continuous treatment at low cost.

DESCRIPTION OF DRAWING(S) - The diagram is a schematic view showing the broken paper pieces.

EQUIVALENT-ABSTRACTS:

TEXTILES AND PAPER

Preferred Method: The paper is broken so that the length of the longest side in at least 50 wt.% of the pieces is 5 mm or less. Preferably the paper fibers are not raised and the length of the shortest side of at least 50 wt.% of the pieces is 0.5 mm or less. The mixing and heating steps are performed using an extruder. The paper material includes at least one of coated paper, resin-composited paper and shredded paper, preferably pulp sludge and the paper is cut so that the ratio of paper fibers of length 1 mm or more is reduced to 20 wt.% or less. The liquefying agent comprises the alkaline or acid catalyst at a ratio of 0.2-10 wt.% relative to the broken paper and the liquid compound at a ratio of 50-300 wt.% relative to the broken paper. Heating is at 100-200 degreesC. The alkaline catalyst is selected from alkaline metal hydroxide, alkaline-earth metal hydroxide, alkaline earth metal carbonate, ammonia and amino compound. The acidic catalyst is selected from sulfuric acid, hydrochloric acid, toluenesulfonic acid, phenol sulfonic acid, aluminum chloride, zinc chloride and boron trifluoride.

POLYMERS

Preferred Components: The hydroxyphenyl compound is selected from phenol, cresol, xlenol, resorcinol, acrylic resorcinol and bisphenol A. The polyol is selected from ethylene glycol, propylene glycol, trimethylene glycol, 1,4-butanediol, 1,5-pentanediol, 1,6-hexanediol, 1,2-hexanediol, 2,4-hexanediol, 1,7-heptanediol, 1,8-octanediol, 1,9-nonanediol, 1,10-decanediol, pinacol, cyclopentane-1,2-diol, cyclohexane-1,4-diol, polyethyleneglycol, polyoxypropylene glycol, polyoxypropylene-polyoxyethylene glycol, glycerin, trimethylolpropane, triethanolamine, 1,2,6-hexanetriol, pentaerythritol, methyl glucoside, sorbitol, mannitol and sucrose. The cyclic ester is selected from propionolactone, beta-butyrolactone, alpha,alpha'-bischloromethylpropionolactone, alpha,alpha-dimethyl-beta-propionolactone, delta-valerolactone, 1,4-dioxan-2-one, glycolide, trimethyl carbonate, neopentyl carbonate, ethylene oxalate, propion oxalate, epsilon-caprolactone, alpha-methyl-epsilon-caprolactone, beta-methyl-epsilon-caprolactone, gamma-methyl-epsilon-caprolactone, 4-methyl-7-isopropyl-epsilon-caprolactone, 3,3,5-trimethyl-epsilon-caprolactone, cis-disalicylide and trisalicylide.

Used A4 paper sheets recovered from OA devices were placed in a shear cutting machine to give pieces of paper in which 99 wt.% or more of the pieces had the length of the longest side being 2 mm or less and the thickness being 0.2 mm or less. A bench extruder was used to adjust the temperature to 170 degreesC and used paper pieces (100 parts weight (pts. wt.)), polyethylene glycol of average molecular weight 400 (140 pts. wt.), glycerin (60 pts. wt.) and sulfuric acid (6 pts.

wt.) were extruded together. After 15 minutes a black-colored liquefied product began to flow out continuously. The product had 8% residue (weight of residue/weight of raw paper x 100), 2.6% residue content (weight of residue/weight of liquefied product x 100) and a viscosity of 41 P. In a comparative example the paper pieces had a width of 5 mm and were then cut using scissors to give less than 1% of pieces which had a longest side of 5 mm or less. It was difficult to feed the mixture into an extruder and hence liquefaction of the paper did not proceed.

CHOSEN-DRAWING: Dwg.1/1

TITLE-TERMS: METHOD LIQUEFY BREAK PAPER
MATERIAL MANUFACTURE PLASTIC

DERWENT-CLASS: A11 A28 F09 P43 P63

CPI-CODES: A10-D; A11-B01; A12-W06C; F05-A06C;

ENHANCED-POLYMER-INDEXING: Polymer Index [1.1]
018 ; G1558 D01 D23
D22 D31 D42 D50 D73
D82 F47 R00351 444;
G1558 D01 D11 D10 D23
D22 D31 D42 D50 D73
D83 F47 R00370 238;
P0975*R P0964 F34 D01
D10; P8004 P0975 P0964
D01 D10 D11 D50 D82
F34; P8015 P0975 P0964
D01 D10 D11 D50 D83
F34; P0055; H0000;
H0022 H0011;

Polymer Index [1.2]

018 ; Q9999 Q8582;
ND01;

Polymer Index [2.1]
018 ; G1843*R D01 F73;
S9999 S1434; P1592*R
F77 D01; H0011*R;
L9999 L2528 L2506;
L9999 L2824;

Polymer Index [2.2]
018 ; Q9999 Q6791;
N9999 N6439; N9999
N6440*R; N9999
N6177*R; ND07;

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